



Optical turbulence profiling at White Sands Missile Range North Oscura Peak

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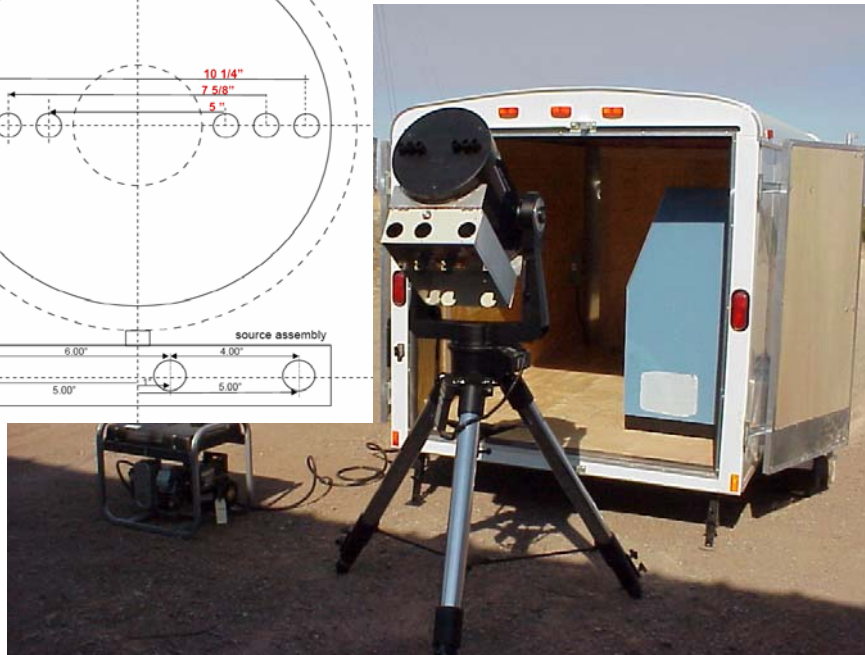
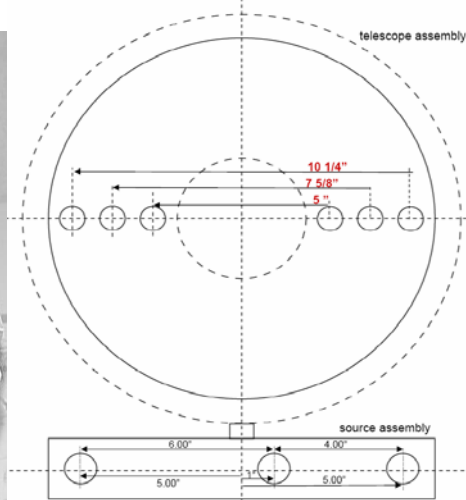
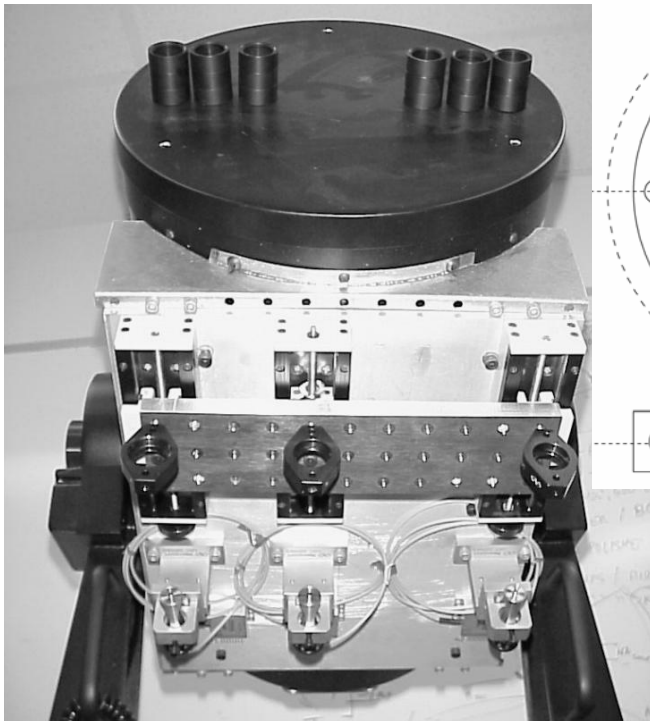
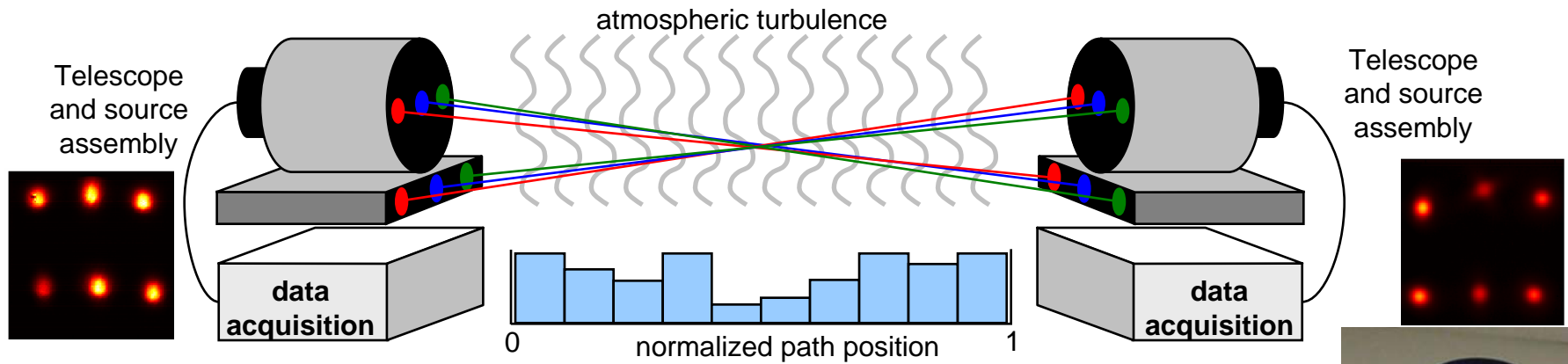
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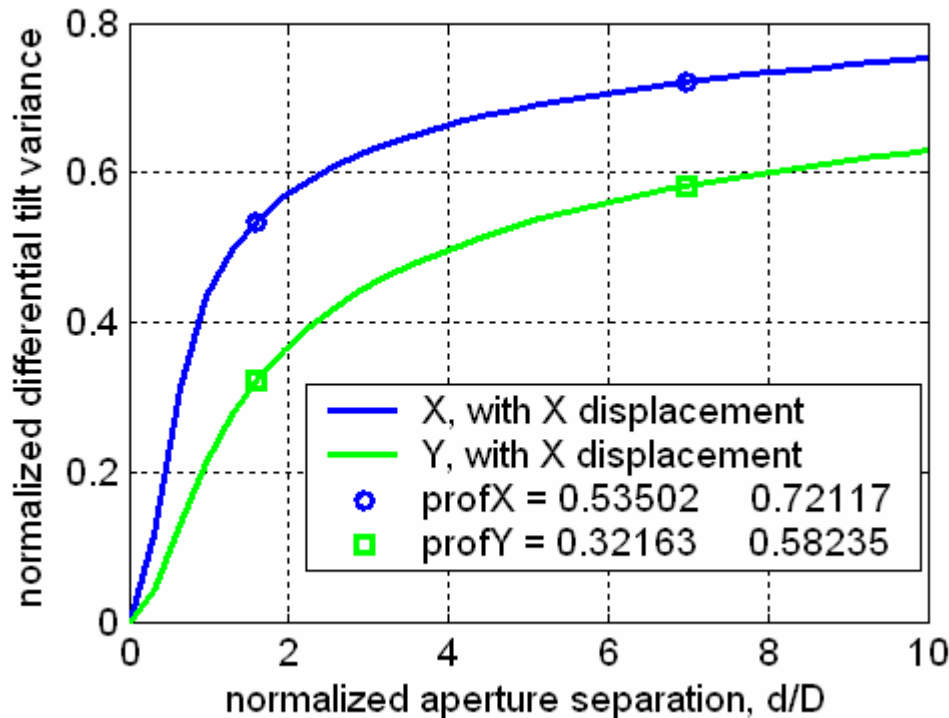
Introduction

- **AFRL Starfire Optical Range owns/operates a device known as the “Differential-Tilt Turbulence Profiler”**
- **Development timeline**
 - 2000: AFRL/DE and AFOSR developed original concept, theory, initial design
 - 2001-2003: AFRL/DE and MZA integrated the laser & optical system, developed data acquisition software
 - 2002-2005: AFRL/DE conducted simulations, developed processing algorithms, initial testing and data analysis
 - 2006: Full-scale system test at North Oscura Peak (NOP)
- **Testing timeline**
 - 2003: NOP to Bug (~1 km), NOP to Beck (~10 km)
 - ◆ Initial data, but issue with source assembly
 - 2004: SOR to 2-mile (~3 km)
 - ◆ Revised source assembly
 - ◆ Reasonable test data and profiling results for 3 km path
 - 2005: NOP to Salinas (~50 km)
 - ◆ Poor SNR limited measurements, profiling questionable
 - 2006: NOP to Beck (~10 km)
 - ◆ Good SNR, reasonable profiles, large data volume, other diagnostics

Differential-Tilt Turbulence Profiler



Estimation of Coherence Diameter from Profiler Centroid Data



- Can use centroid (tilt) data directly from profiler units with standard techniques for r_0 estimation

- Estimation from tilt-variance:

$$\sigma_T^2 = 0.1816 D^{-1/3} \lambda^2 r_0^{-5/3}$$

$$r_0 = \left(\frac{\sigma_T^2 D^{1/3}}{0.1816 \lambda^2} \right)^{-3/5}$$

- Differential-tilt variance for 3 aperture pairs on each unit

- Ap-1 / Ap-2 with $s/D = 1.5875 \rightarrow$

$$\sigma_{\Delta T}^2 = 0.1943 D^{-1/3} \lambda^2 r_0^{-5/3}$$

- Ap-3 / Ap-4 with $s/D = 6.9850 \rightarrow$

$$\sigma_{\Delta T}^2 = 0.2619 D^{-1/3} \lambda^2 r_0^{-5/3}$$

- Ap-5 / Ap-6 with $s/D = 1.5875 \rightarrow$

$$\sigma_{\Delta T}^2 = 0.1943 D^{-1/3} \lambda^2 r_0^{-5/3}$$

Profiler Theory of Operation

- **Profiler theory published in SPIE proceedings**
 - Whiteley, M. R., Washburn, D. C., and Wright, L. A., “Differential-tilt technique for saturation-resistant profiling of atmospheric turbulence,” *SPIE Proceedings on Adaptive Optical Systems Technology II* 4494, (2001).
- **Difference of differential-tilt variances define measurement set that can be related to turbulence distribution over path**

$$\text{continuous: } m_k = \int_0^1 d\xi C_n^2(\xi L) w_{\delta k}(\xi)$$

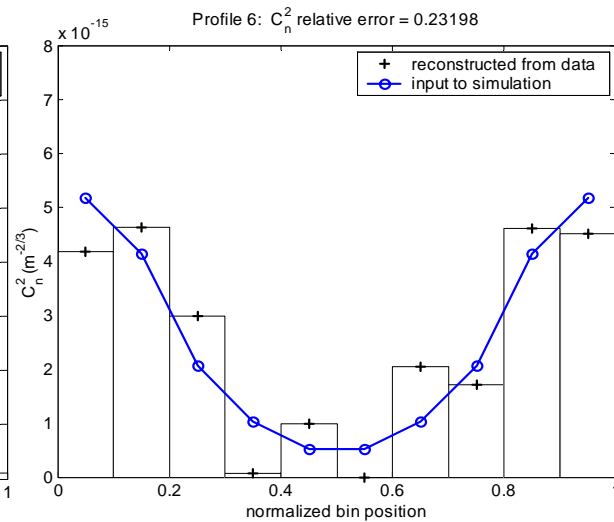
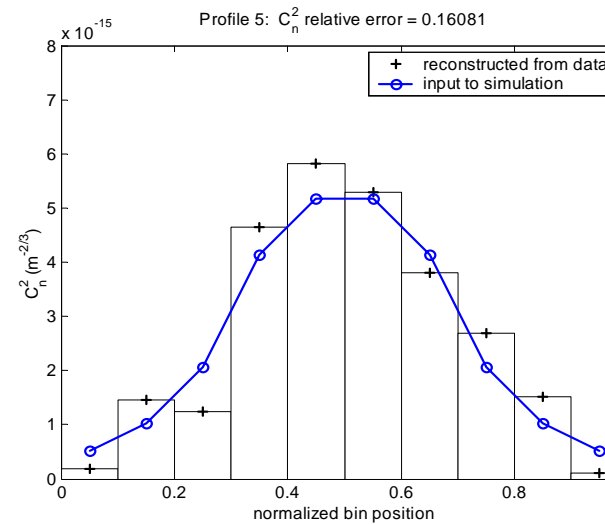
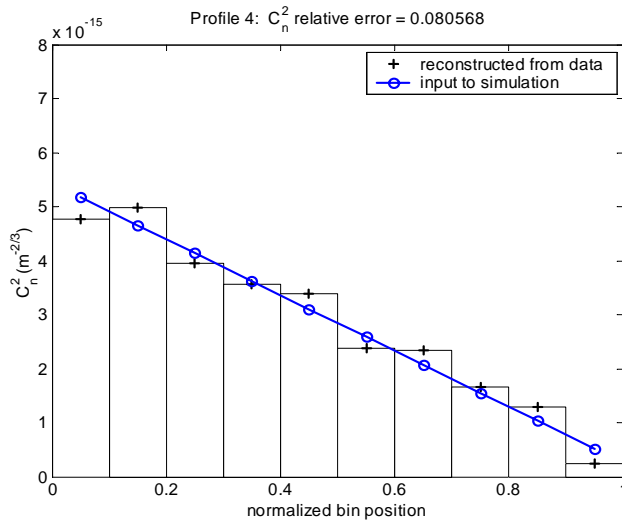
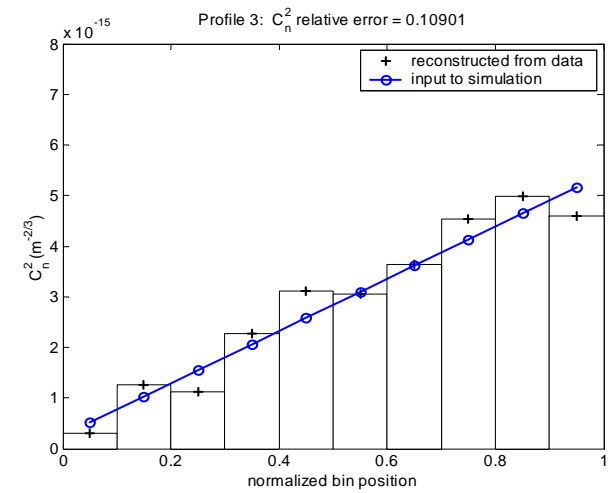
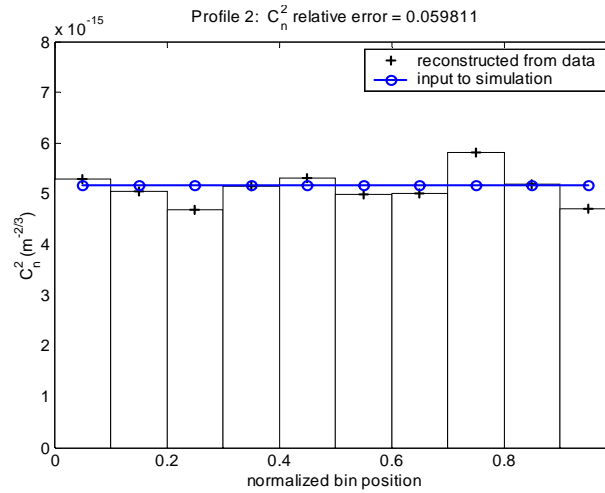
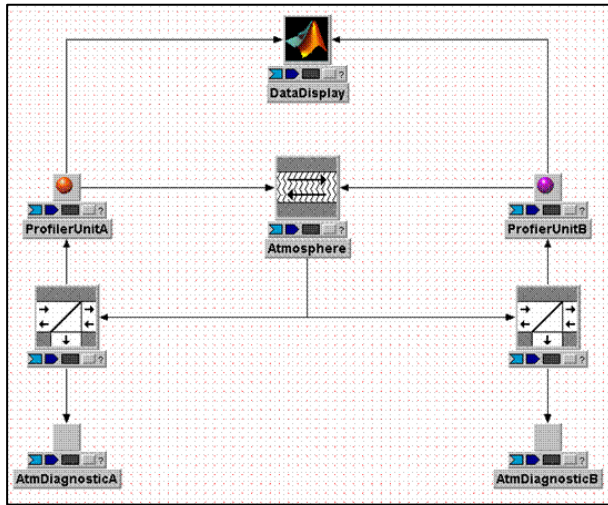
$$\text{discrete: } m_k = \sum_{i=1}^N C_{ni}^2 p_{ki} \rightarrow \mathbf{m} = P\mathbf{c}$$

- **Relation can be inverted through appropriate numerical technique**
- **Constraints can be applied to inversion using r_0 estimates for profiler used as differential-image-motion monitor**

$$\mathbf{c} = (P^T P)^{-1} (P^T \mathbf{m} + \lambda_A \mathbf{w}_{r_A} + \lambda_B \mathbf{w}_{r_B})$$

Wave-Optics Simulation of Turbulence Profiling

WaveTrain System Model



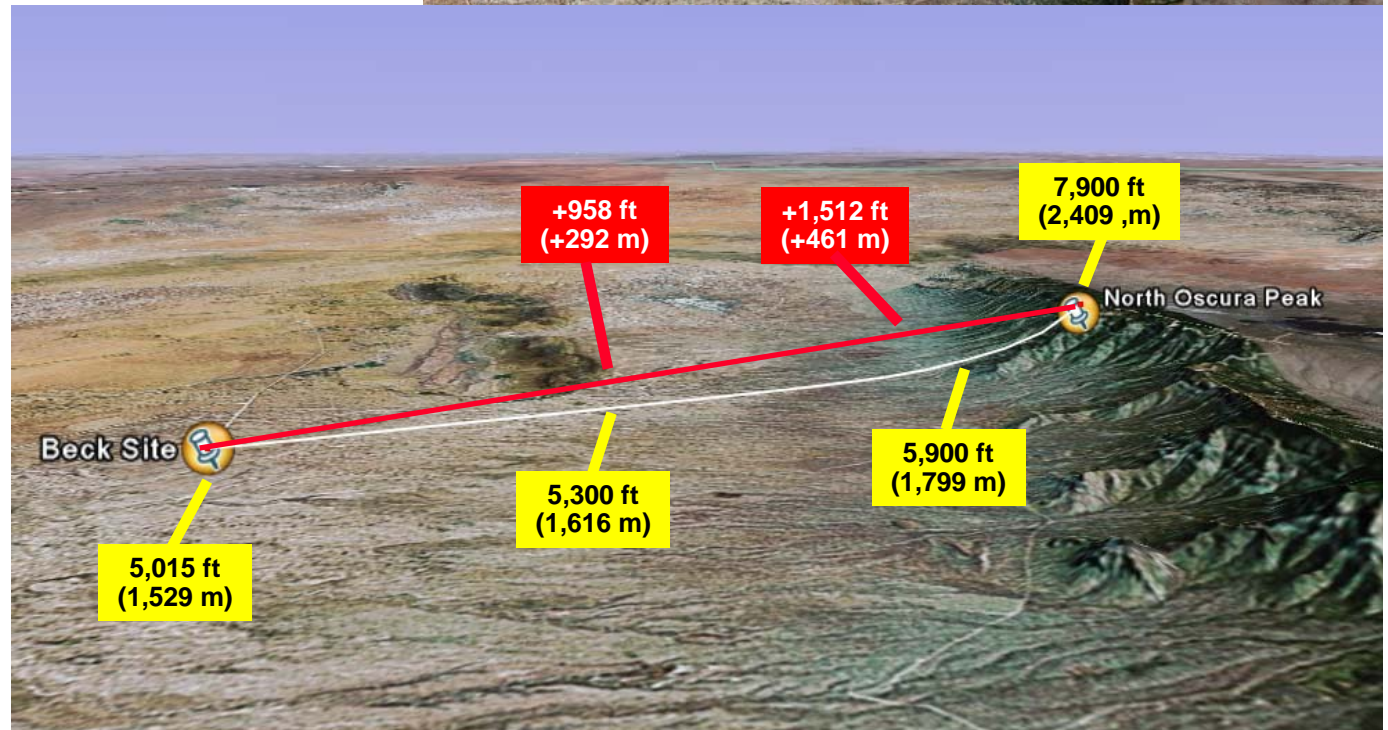
NOP-to-Beck Site Data Collection

- Turbulence profiler data was collected on NOP-to-Beck path

- 9.6 km, ~900 m altitude change
- April-August 2006
- Other data items
 - ◆ Scintillometer
 - ◆ Tactical imagery

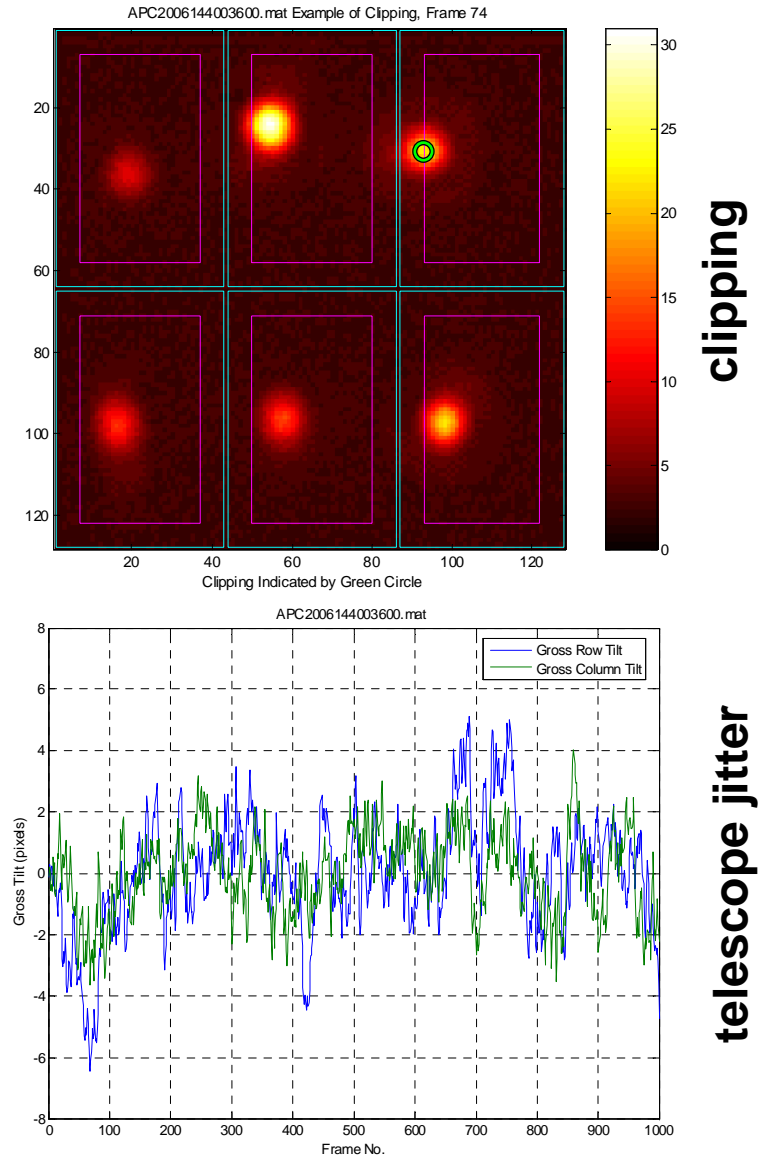


- 33 test days with profiler
- 21 days of good quality/volume for profiling
- ~4500 data files
- 726 profiles
 - 0000-0600: 120
 - 0600-1200: 86
 - 1200-1800: 110
 - 1800-2400: 410

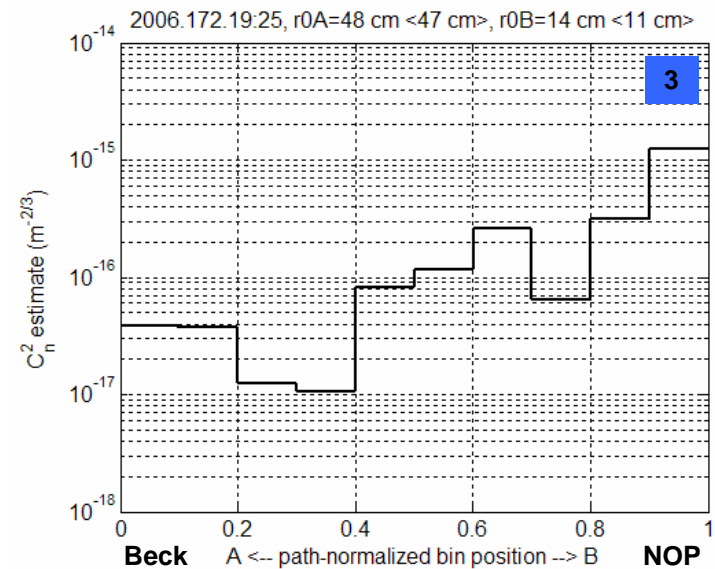
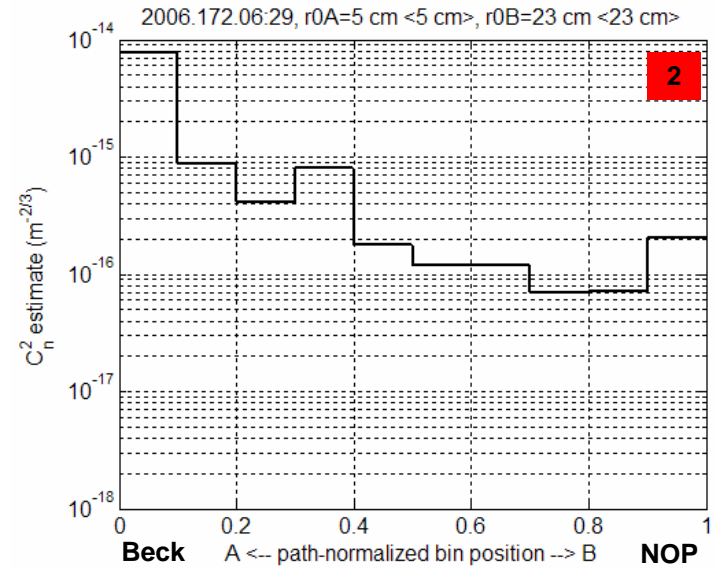
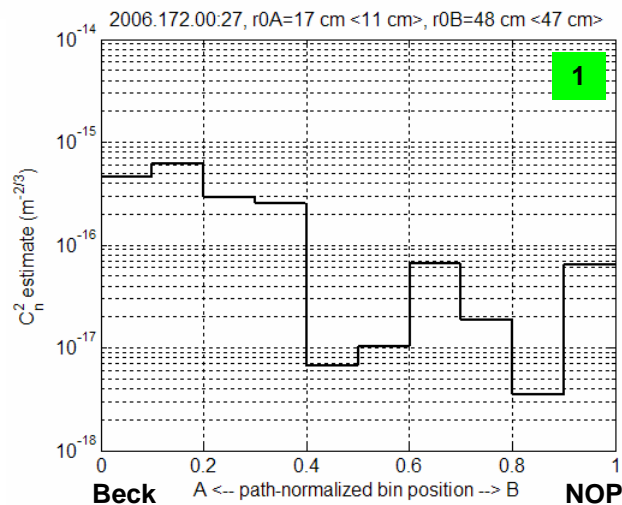
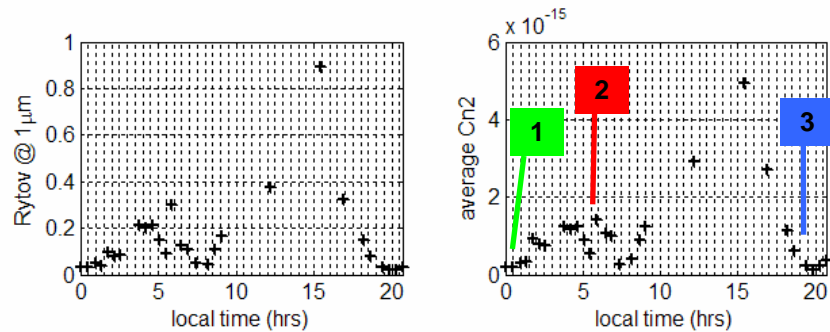
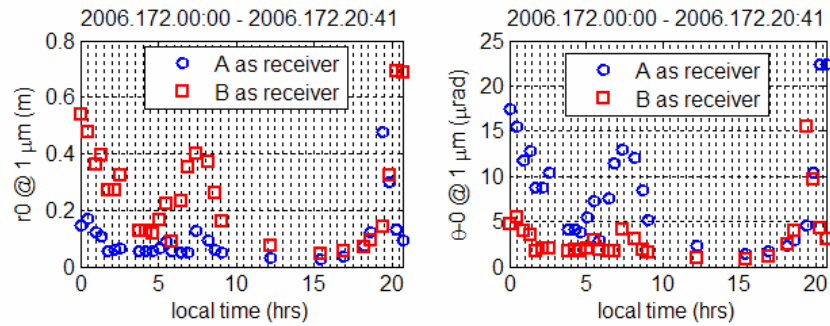


Data Quality Checking

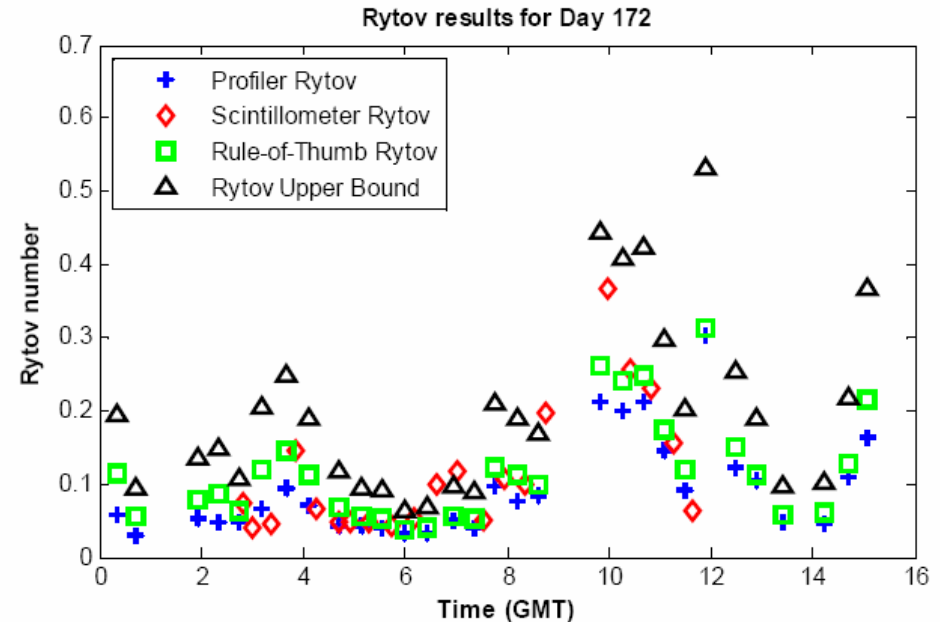
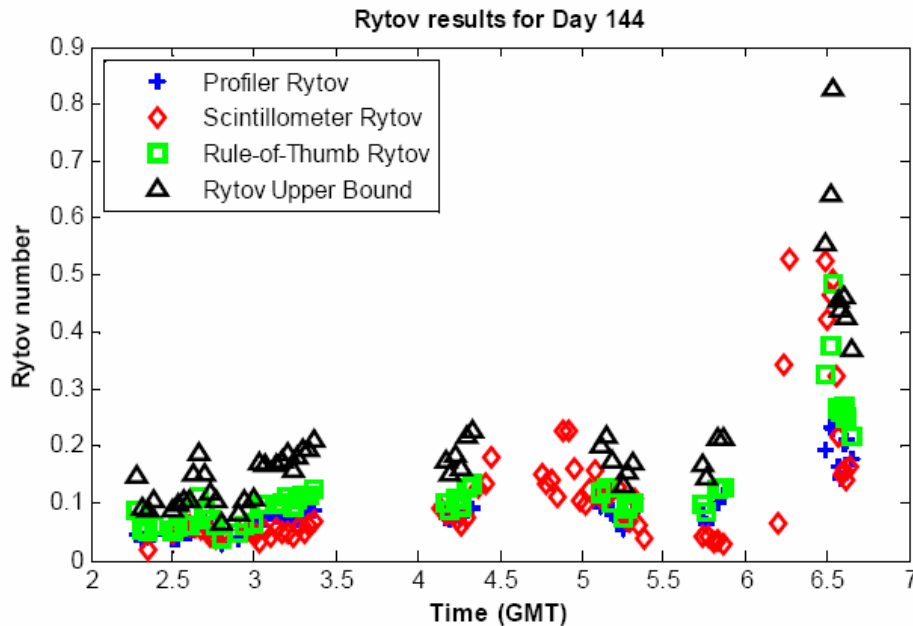
- **Data filtering implemented to reduce noise sources in differential-tilt estimation**
- **Spot SNR**
 - Average pixel SNR ≥ 2 for all subapertures
- **Saturated spot image**
 - No saturated pixels used in centroid
- **Spot clipping**
 - Subaperture spot too close to centroid processing boundary
- **Telescope jitter**
 - Quantified by averaging shift over all subapertures
 - Retained data with jitter std < 7 pixels
- **Required following attributes for profile processing**
 - At least 10% of frames in a file must pass all quality checks
 - At least 200 frames total passing quality checks
- **SNR was most common reason for data filtering**
 - Especially when scintillation was high



Profiling Example: Day 172



Comparison with Scintillometer



- Rytov number from turbulence profiles compared with scintillometer estimate of Rytov number (when available)
- It can be shown that for any turbulence profile, the following inequality applies:

$$\mathcal{R} \leq \frac{1}{9.1314} \left(\frac{\lambda}{r_0 \theta_0} \right)^{5/6}$$

$$\mathcal{R} \simeq 15.53^{-1} \left(\frac{\lambda}{r_0 \theta_0} \right)^{5/6}$$

- A good “rule of thumb” approximation is:
- When scintillometer is in bounds implied by profiler, scintillometer and profiler give consistent Rytov number estimates

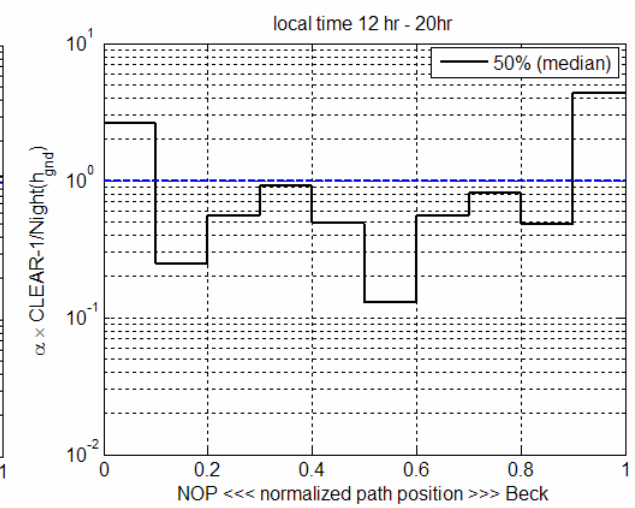
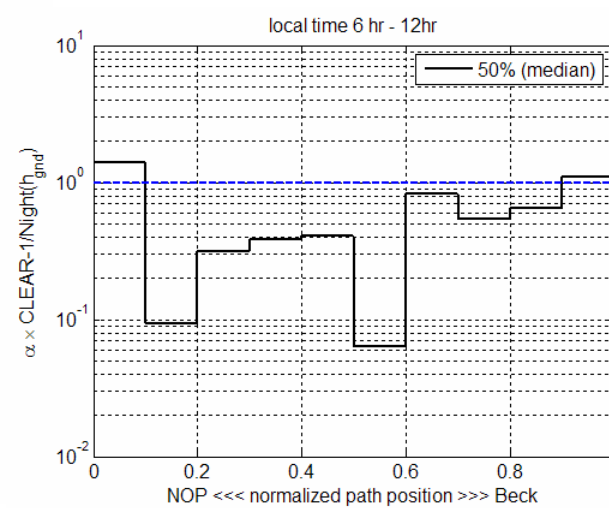
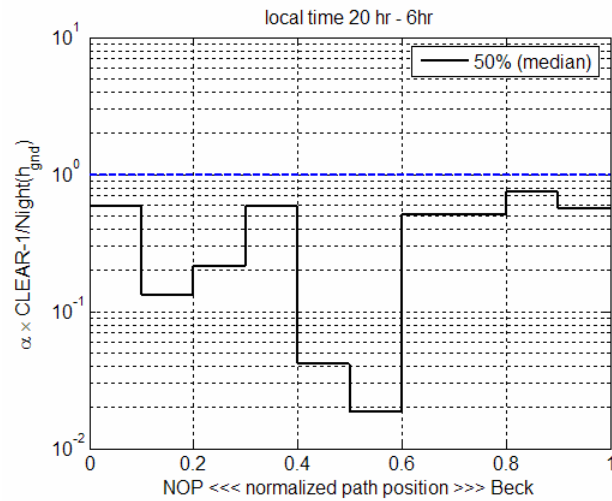
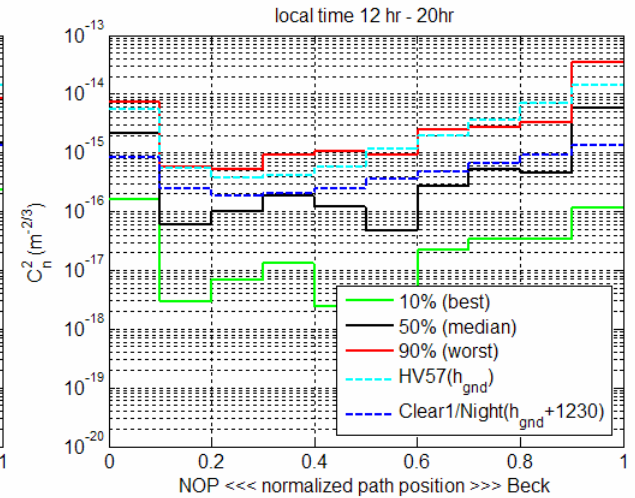
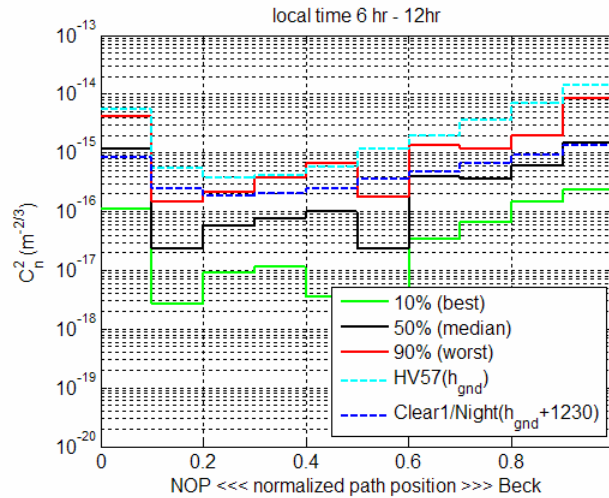
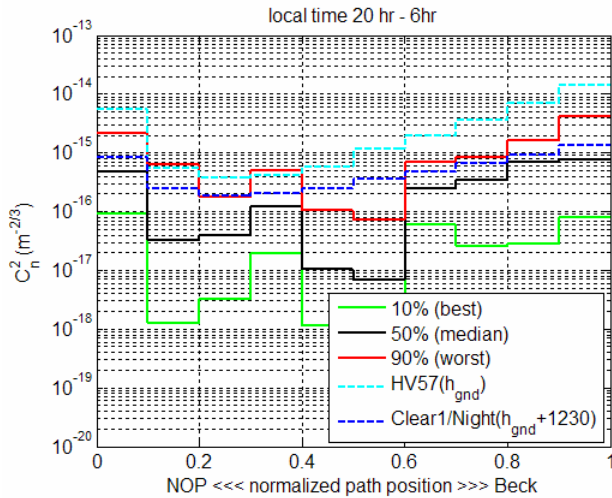


Comparison with Standard Turbulence Models

“Night” 20:00-06:00

“Morning” 06:00-12:00

“Afternoon” 12:00-20:00



Conclusions

- **Differential-tilt turbulence profiler successfully taken from concept to development and into application**
 - ~10 km path from North Oscura Peak to valley floor at WSMR
- **Substantial test data has been collected and analyzed**
 - Filtering for data quality important to assuring turbulence estimate
 - Profile estimates available around the clock
 - Profiles and derived atmospheric propagation parameters consistent with expected trends
- **Profile estimates validated using independent measurements**
 - Consistency between profile Rytov and scintillometer
- **Diurnal trends (median conditions)**
 - Compare favorably to CLEAR-1 model given propagation height above ground
 - Night
 - ◆ $< 0.5 \times \text{CLEAR-1/Night}$
 - Morning
 - ◆ $0.5 - 1.0 \times \text{CLEAR-1/Night}$
 - Afternoon
 - ◆ End-points (near ground) $2.0 - 4.0 \times \text{CLEAR-1/Night}$
 - ◆ Otherwise, $0.5 - 1.0 \times \text{CLEAR-1/Night}$